How to model the Surface boundary Layer and/or canopy processes?

with a 1D turbulence scheme inside Surface schemes !

Valéry MASSON, Rafiq HAMDI, Yann SEITY





SBL scheme principle : state of the art







SBL scheme principle : what we want to do



"single-layer" surface scheme + Surface Boundary Layer scheme forced offline "single-layer" surface scheme + Surface Boundary Layer scheme coupled to an atmospheric model "multi-layer" surface scheme coupled to an atmospheric model





• Evolution equations in the SBL are :

$$\begin{array}{rcl} \frac{\partial U}{\partial t} &=& Adv + Cor &+ Pres. &+ Turb(U) &+ Drag_{u} \\\\ \frac{\partial V}{\partial t} &=& Adv &+ Cor &+ Pres. &+ Turb(V) &+ Drag_{v} \\\\ \frac{\partial \theta}{\partial t} &=& Adv &+ Diab. &+ Turb(\theta) &+ \frac{\partial \theta}{\partial t}_{canopy} \\\\ \frac{\partial q}{\partial t} &=& Adv &+ Turb(q) &+ \frac{\partial q}{\partial t}_{canopy} \end{array}$$

$$\frac{\partial e}{\partial t} = Adv + Dyn.Prod. + Therm.Prod. + Turb + Diss. + \frac{\partial e}{\partial t}_{canopy}$$





• Regrouping terms into 3 main types :

$$\frac{\partial U}{\partial t} = LS(U) + Turb(U) + Drag_{u}$$
$$\frac{\partial V}{\partial t} = LS(V) + Turb(V) + Drag_{v}$$
$$\frac{\partial \theta}{\partial t} = LS(\theta) + Turb(\theta) + \frac{\partial \theta}{\partial t}_{canopy}$$
$$\frac{\partial q}{\partial t} = LS(q) + Turb(q) + \frac{\partial q}{\partial t}_{canopy}$$

The TKE equation remains the same:

$$\frac{\partial e}{\partial t} = Adv(e) + Dyn.Prod. + Therm.Prod. + Turb + Diss. + \frac{\partial e}{\partial t_{canopy}}$$





- Supposing that:
 - The mean wind direction does not vary with height in the SBL
 - The turbulent transport and advection of TKE is small in the SBL compared to other terms
 - Above the canopy (if any), the turbulent fluxes are uniform with height (« constant flux layer »)
 - The Large-Scale Forcing terms LS(U), LS(θ), LS(q) are uniform with height in the SBL

 \rightarrow These are hypotheses commonly done in Monin-Obukhov-like SBL relationships

$$\frac{\partial U}{\partial t} = \frac{\partial U}{\partial t}(z = z_a) + Turb(U) + Drag_u$$
$$\frac{\partial \theta}{\partial t} = \frac{\partial \theta}{\partial t}(z = z_a) + Turb(\theta) + \frac{\partial \theta}{\partial t}_{canopy}$$
$$\frac{\partial q}{\partial t} = \frac{\partial q}{\partial t}(z = z_a) + Turb(q) + \frac{\partial q}{\partial t}_{canopy}$$

$$\frac{\partial e}{\partial t} = Dyn.Prod. + Therm.Prod. + Diss. + \frac{\partial e}{\partial t_{canopy}}$$





SBL canopy scheme in TEB

- Offline Validation with the BUBBLE data
 - City-center of Basel (Switzerland)
 - Simulation covers half of the summer IOP: from 16th to 30th June, 2002

Basel-Sperrstrasse







SBL canopy scheme in TEB

- Dynamical variables
 - Walls imply a drag force on the flow parameterized (CD=0.4) as : Cd U^2
 - Walls are also a source of TKE, parameterized as : + Cd U³
 - Both mean wind profile and momentum fluxe profile are correctly simulated



SBL canopy scheme in TEB





Evaluation on July 2007 and January 2007 on South East France domain :

5 levels added + turbulence scheme used







Scores in plains (z<300m)



Scores in mountaineous areas



Better statistical scores, Especially in mountains

No surface/atmosphere decoupling \downarrow Significant (negative) heat fluxes \downarrow Air cooling in the atmospheric model \downarrow Better catabatic winds \downarrow Better structure of temperature field







- One 1D SBL & « canopy » scheme has been included in SURFEX
- This allows a better physical treatment of the SBL, taking into account obstacle effects if any (e.g. buildings in TEB)
- Scores are globally improved, especially over mountains
- To couple the surface scheme (ISBA) with a very low SBL level avoids the classical surface/atmosphere decoupling
- Opens new collaboration opportunities on e.g. forest schemes including a tree canopy







Thank you





- Turbulence scheme is the Cuxart, Bougeault, Redelsperger (2000)
- Mixing and dissipative length scale, above canopy, are given by Redelsperger, Mahé and Carlotti 2001

A summary of the turbulence scheme is given below:

$$\begin{cases}
\overline{u'w'} = -C_u l \sqrt{e} \frac{\partial U}{\partial z} \\
\overline{w'\theta'} = -C_{\theta} l \sqrt{e} \frac{\partial \theta}{\partial z} \\
\overline{w'q'} = -C_q l \sqrt{e} \frac{\partial q}{\partial z} \\
\frac{\partial e}{\partial t} = \underbrace{-\overline{u'w'}}_{Dyn.Prod.} \frac{\partial U}{\partial t} + \underbrace{\frac{g}{\theta} \overline{w'\theta'_v}}_{Therm.Prod.} - \underbrace{C_{\epsilon} \frac{e^{\frac{3}{2}}}{l_{\epsilon}}}_{Diss.} + \frac{\partial e}{\partial t \, canopy} \\
\end{cases}$$
(10)

with $C_u = 0.126, \ C_{ heta} = C_q = 0.143, \ C_{\epsilon} = 0.845$ (from Cheng et al 2002 constants

values for pressure correlations terms and using Cuxart et al 2000 derivation). The mixing and dissipative lengths, l and l_{ϵ} respectively, are equal to (from Redelsperger et al 2001, $\alpha = 2.42$):

$$\begin{cases} l = \kappa z / [\sqrt{\alpha} C_u \phi_m^2 (z/L_{MO}) \phi_e(z/L_{MO})]^{-1} \\ l_\epsilon = l \alpha^2 C_\epsilon / C_u / (1 - 1.9z/L_{MO}) & \text{if } z/L_{MO} < 0 \end{cases}$$
(11)
$$l_\epsilon = l \alpha^2 C_\epsilon / C_u / (1 - 0.3\sqrt{z/L_{MO}}) & \text{if } z/L_{MO} > 0 \end{cases}$$

Where L_{MO} is the Monin-Obukhov length, ϕ_u and ϕ_e the Monin-Obukhov stability functions

for momentum and TKE.



