



Met Office

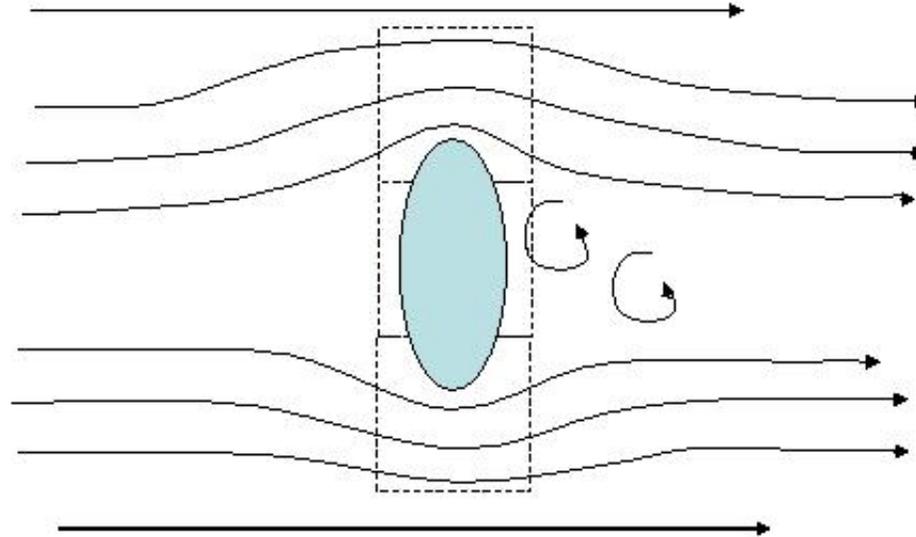
# Grid-scale forcing and its effect on larger scales in environmental flows

Terry Davies Dynamics Research

## Under-resolved flows

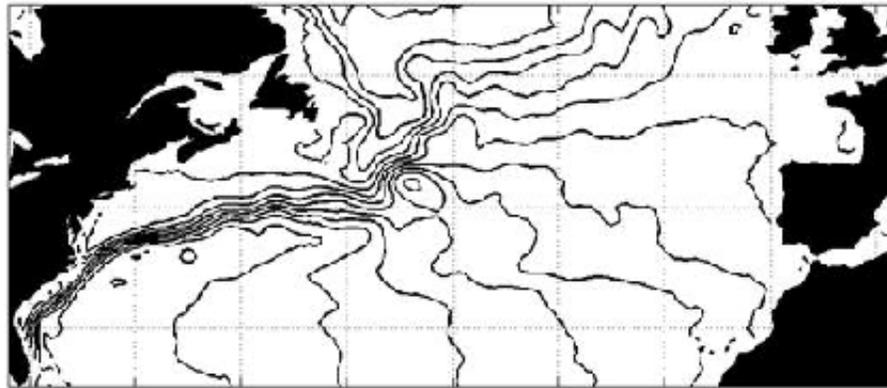
- Relevant processes at and below the grid-scale are typically parametrized. i.e. generally a column calculation using the large scale variables, model parameters and empiricism for a fixed time step. The model dynamics cannot properly represent processes at or below the grid-scale (in fact below scales of several grid lengths ) and yet the coupling between dynamics and physics is essentially at the grid-scale.
- Models of real flows over obstacles are always under resolved unless the obstacle has a smooth shape i.e. the minimum variation on the surface of the obstacle is several grid-lengths.
- Terrain and coasts are “fractal-like”. Increasing resolution introduces new features.
- Edges and corners are always under-resolved.

# FLOW AROUND SUB-GRID OROGRAPHY

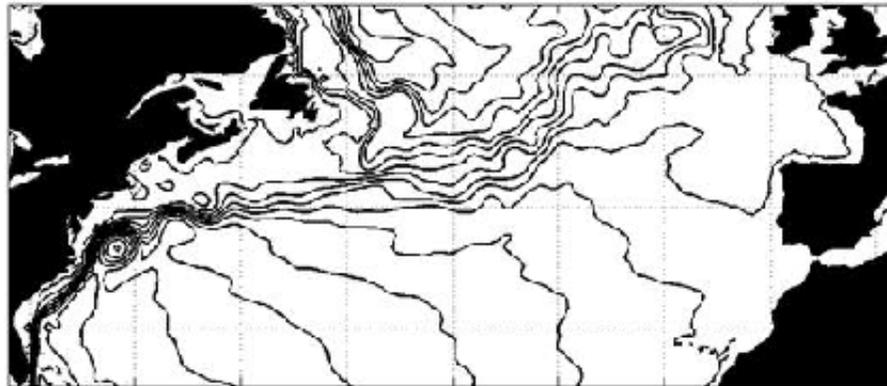


Sea Surface Height

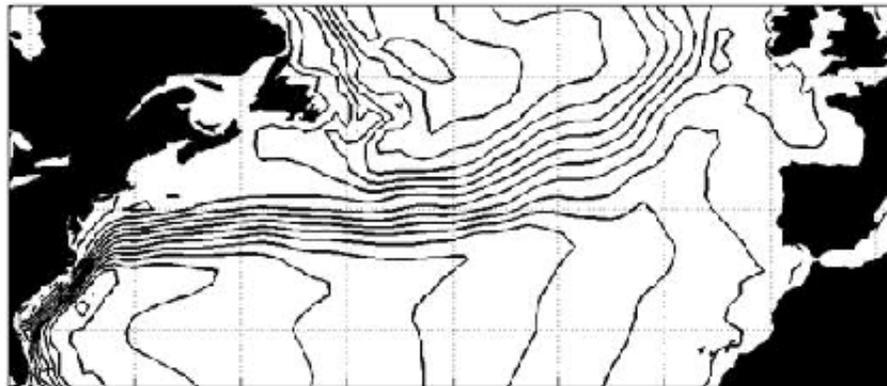
Observations



HiGEM



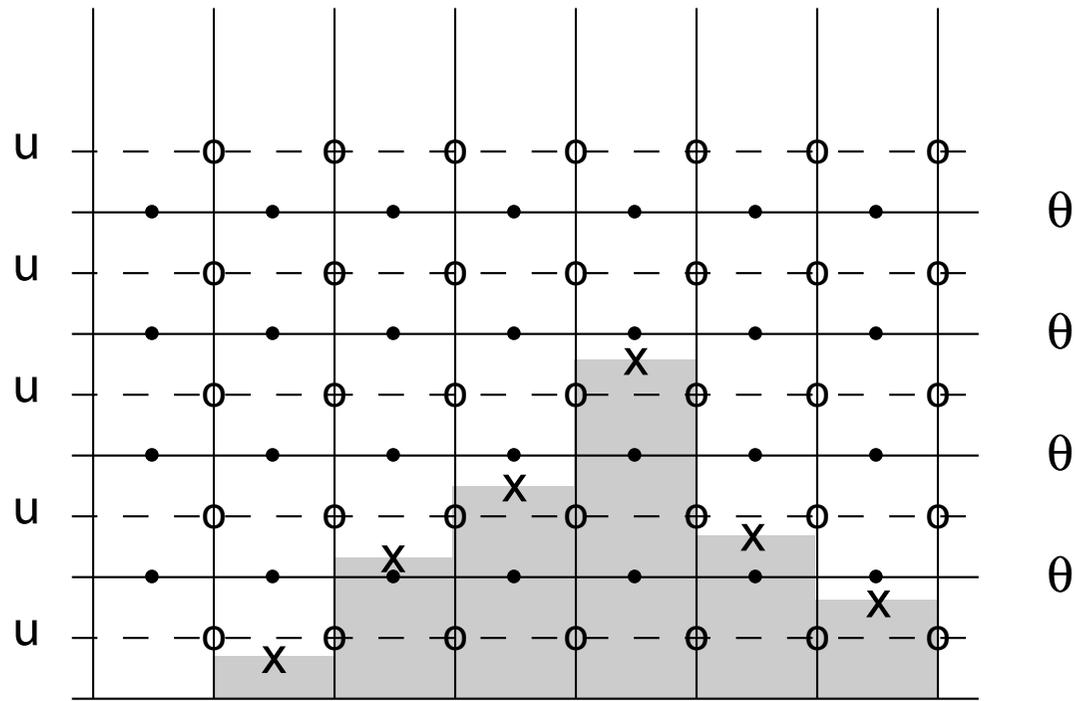
HadGEM



## Terrain-following coordinates

- Most widely used in NWP and climate models.
- Easy to apply lower boundary condition but....
- Horizontal pressure gradient terms consists of 2 parts which for steep slopes are of similar magnitude but opposite signs. i.e. actual horizontal pressure gradient is a small residual between 2 terms. Flattening the coordinates so that they are horizontal above a certain altitude helps (Hybrid coordinates).
- For C-grid staggering, the horizontal winds in the vertical Coriolis terms need to be averaged and near steep slopes the horizontal wind components on the same model ( $\eta$ ) levels will be at different heights.
- Terrain-following coordinates not suitable for large aspect ratios hence interest in shaved/cut cells etc. But these have yet to make it into operations.

# VERTICAL GRID



## How to block flow (consistently)

Consider

$$\frac{\partial u}{\partial t} = -K(\mathbf{x}, \mathbf{u}) u, \quad (1)$$

where  $K = K(\mathbf{x}, \mathbf{u})$ , i.e  $K$  depends on position and flow (and resolution!).

$K = 0$  represents the undisturbed state.

The solution is  $u = u_0 \exp(-K(\mathbf{x}, \mathbf{u}) t)$ .

For very large  $K$ ,  $u \rightarrow 0$  and equation (1) can be recast as

$$u = -\frac{\partial u}{\partial t} / K$$

which has the appropriate asymptotic behaviour.

Thus, adding a term as in equation (1), provides a mechanism for blocking flow.

Can this be done for the momentum equations and can it be justified?

## Time-averaged Navier-Stokes equations

$u = \bar{u} + u'$  where  $u' \ll \bar{u}$  and  $\bar{u} = \int^T u dt$  and  $\int^T u' dt = 0$ ,

$$\frac{d\bar{u}}{dt} = \frac{1}{\rho} \frac{\partial p}{\partial x} + f_r \bar{v} + \frac{1}{\rho} \frac{\partial}{\partial x} (-\rho \overline{u'u'}) + \frac{1}{\rho} \frac{\partial}{\partial y} (-\rho \overline{v'u'}) + \frac{1}{\rho} \frac{\partial}{\partial z} (-\rho \overline{w'u'})$$

where,  $f_r = 2\Omega \sin\phi$  and  $\Omega$  is the Earth's angular speed of rotation.

Similarly for  $v, w$  velocity components.

The over-bar for the time-averaged velocity components will be omitted from subsequent slides.

## Additional and/or alternative stress terms

$$\frac{1}{\rho} \frac{\partial}{\partial x} (-\rho \overline{u'u'}) = -K_u(\mathbf{x}, \mathbf{u}, t) u \quad \text{and} \quad \overline{v'u'} = \overline{w'u'} = 0.$$

Similarly for  $v$  and  $w$  equations.

Then

$$\begin{aligned} \frac{du}{dt} - f_r v + \frac{1}{\rho} \frac{\partial p}{\partial x} &= -K_u(\mathbf{x}, \mathbf{u}, t) u \\ \frac{dv}{dt} + f_r u + \frac{1}{\rho} \frac{\partial p}{\partial y} &= -K_v(\mathbf{x}, \mathbf{u}, t) v \\ \frac{dw}{dt} + g + \frac{1}{\rho} \frac{\partial p}{\partial z} &= -K_w(\mathbf{x}, \mathbf{u}, t) w \end{aligned}$$

The interaction coefficients  $K = K(\mathbf{x}, \mathbf{u}, t)$  depend on time, position and flow so these equations cannot be easily solved in this form.

## Solving the new equations

Solving over a (short) time interval  $\Delta t$  for which  $K = K(\mathbf{x}, \mathbf{u})$ , i.e. it depends on position and flow, then

$$\frac{\partial u}{\partial t} = -K(\mathbf{x}, \mathbf{u}) u$$

has the solution  $u = u_0 \exp(-K(\mathbf{x}, \mathbf{u}) \Delta t)$ .

The time discretized equations can be written as

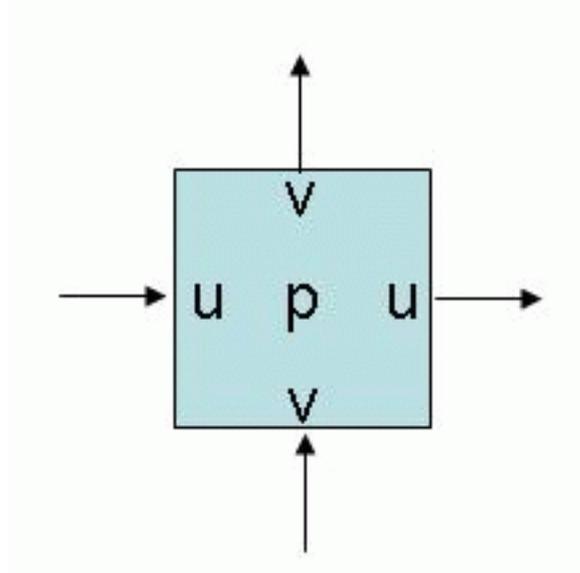
$$(1 + \beta K \Delta t) u^{n+1} = (1 - \alpha K \Delta t) u^n$$

or

$$u^{n+1} = \frac{(1 - \alpha K \Delta t)}{(1 + \beta K \Delta t)} u^n$$

where  $\alpha + \beta = 1$ .  $\alpha = \beta = 1/2$  is  $\mathcal{O}(\Delta t^2)$ , (Crank-Nicholson), whereas  $\alpha = 0$ ,  $\beta = 1$  (fully implicit) is  $\mathcal{O}(\Delta t)$ . However, for  $K \rightarrow \infty$ , only the implicit discretization behaves as the analytic solution, i.e.  $u = 0$ .

## Blocked flow and staggering



For a blocked flow require that normal velocity at a cell face = 0.

C-grid staggering is the natural (only) grid arrangement to do this.

## Applying to New dynamics

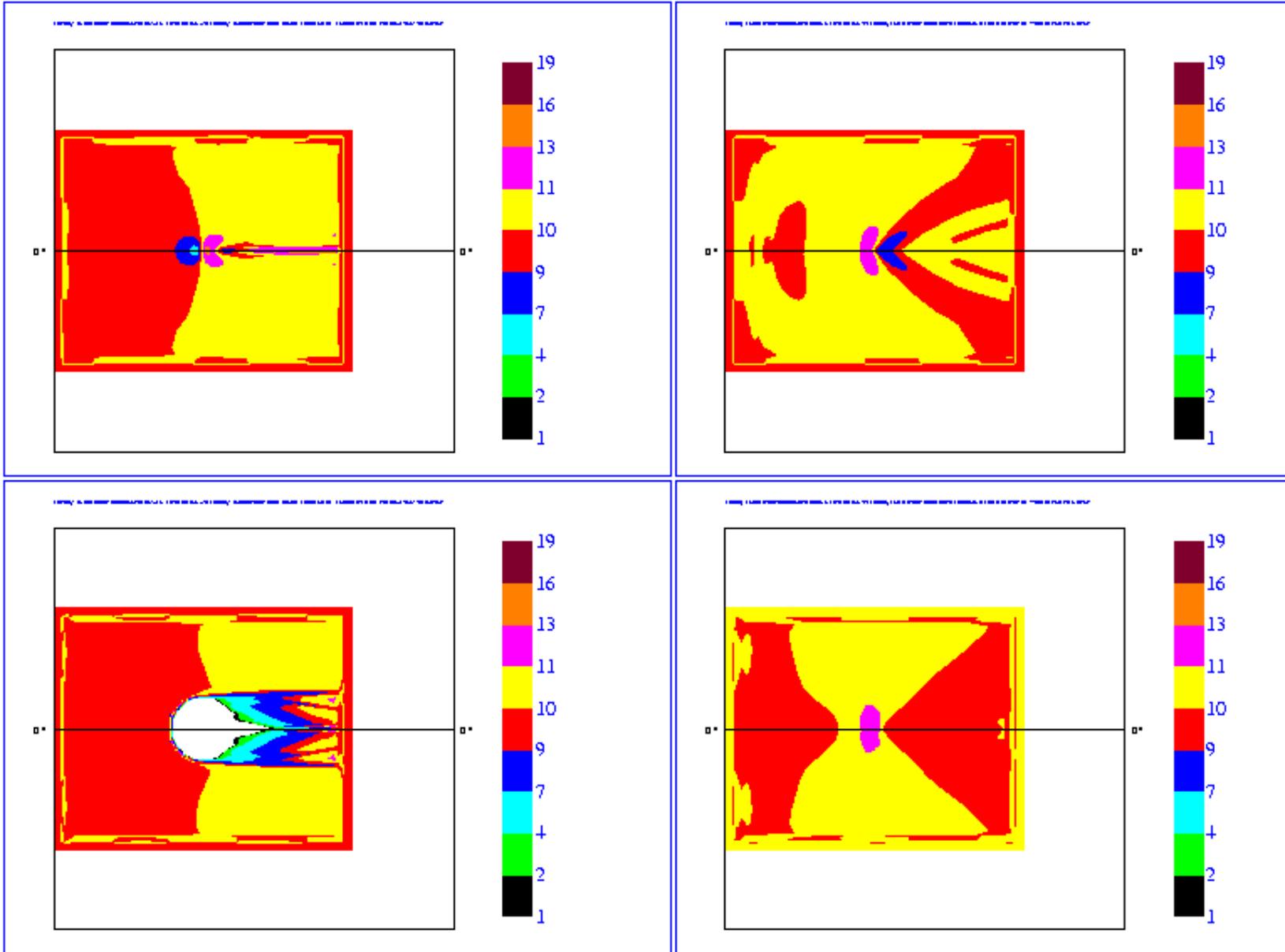
The three stages of the UM predictor-corrector scheme can be written as

$$\begin{aligned}
 (1 + K\Delta t) \mathbf{X}^{(1)} &= \mathbf{X}_d^n + (1 - \alpha)\Delta t(\mathbf{L} + \mathbf{N})_d^n \\
 &\quad + \Delta t (\mathbf{S}_1)_d^n + \alpha\Delta t(\mathbf{L} + \mathbf{N})^n \\
 \mathbf{X}^{(2)} &= \mathbf{X}^{(1)} + \Delta t \mathbf{S}_2(\mathbf{X}^n, \mathbf{X}^{(1)}, \mathbf{X}^{(2)}) \\
 (1 + K\Delta t) \mathbf{X}^{(3)} - \alpha\Delta t \mathbf{L}^{(3)} &= \mathbf{X}^{(2)} + \alpha\Delta t(\mathbf{N}^* - \mathbf{N}^n - \mathbf{L}^n) + K\Delta t \mathbf{X}^{(1)}
 \end{aligned}$$

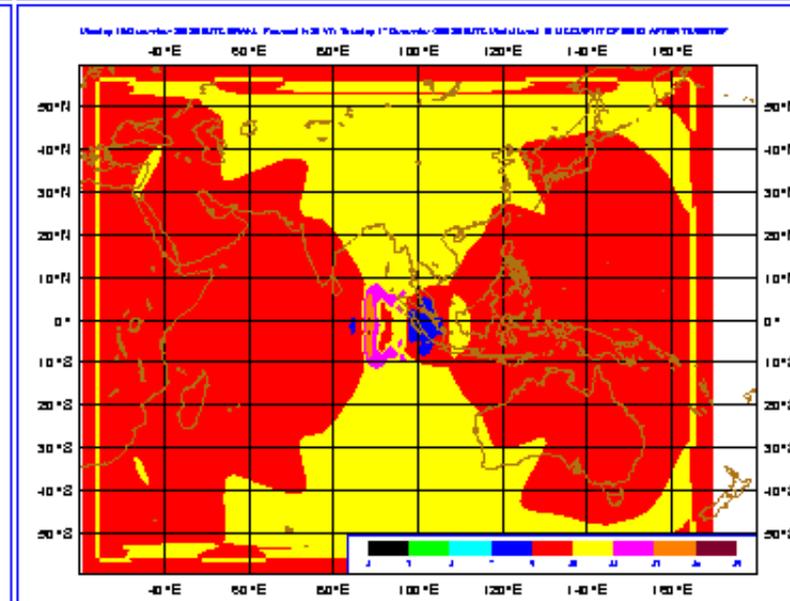
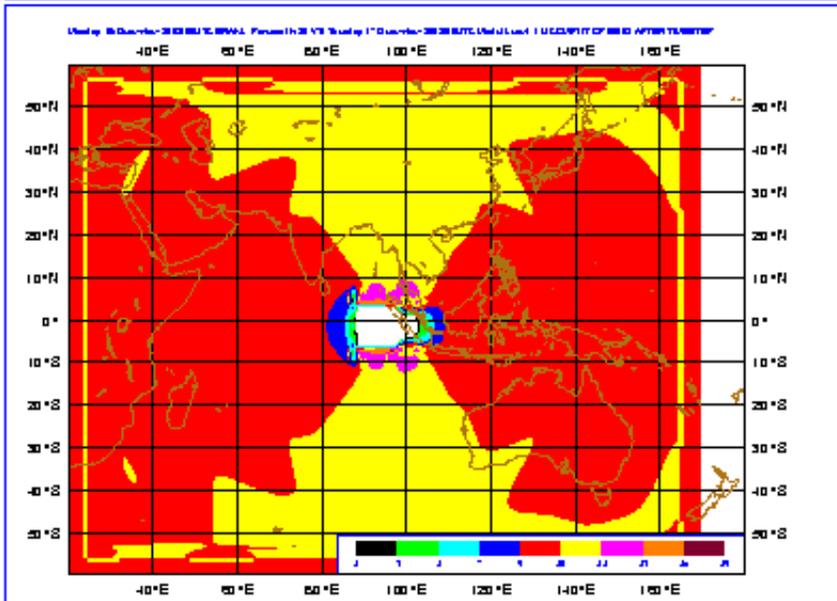
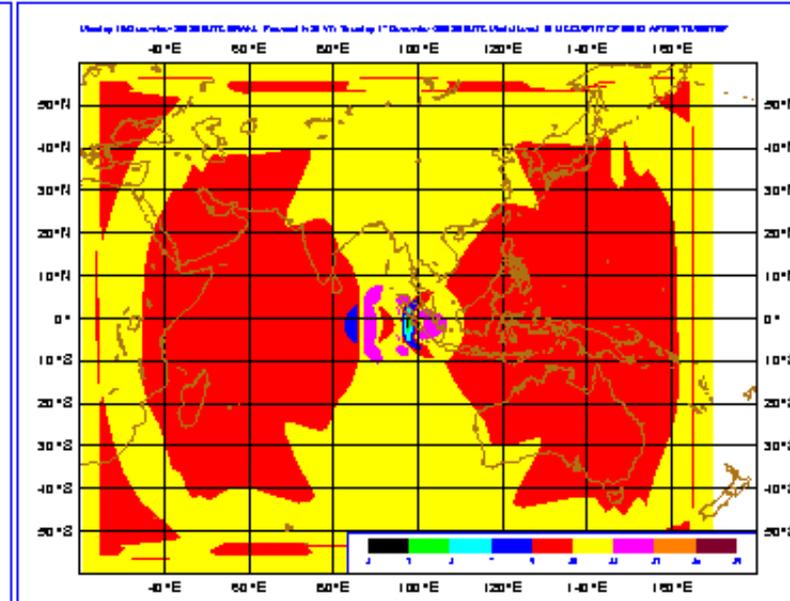
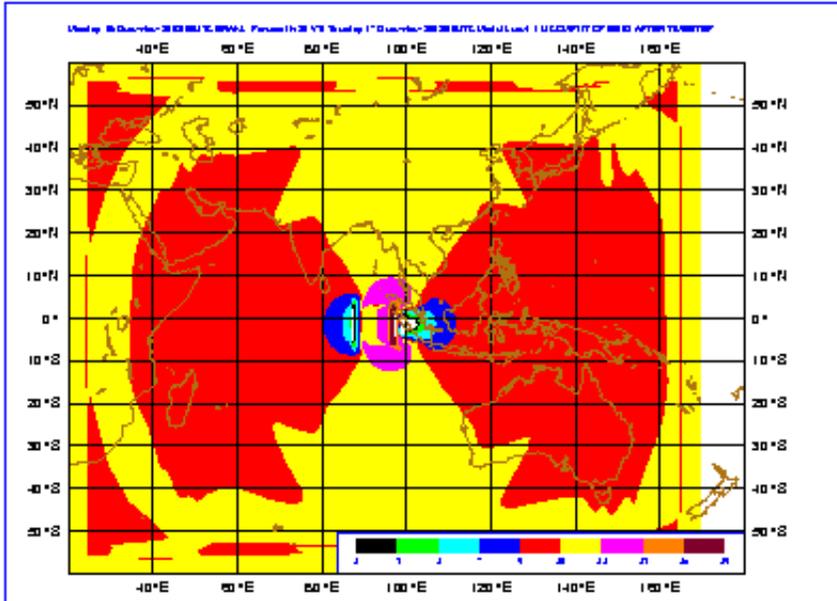
which can be combined to give the target scheme as

$$\begin{aligned}
 \mathbf{X}^{n+1} &= \mathbf{X}_d^n + (1 - \alpha)\Delta t(\mathbf{L} + \mathbf{N})_d^n + \Delta t (\mathbf{S}_1)_d^n + \alpha\Delta t(\mathbf{L}^{n+1} + \mathbf{N}^*) \\
 &\quad + \Delta t \mathbf{S}_2(\mathbf{X}^n, \mathbf{X}^{(1)}, \mathbf{X}^{(2)}) - K\Delta t \mathbf{X}^{n+1}
 \end{aligned}$$

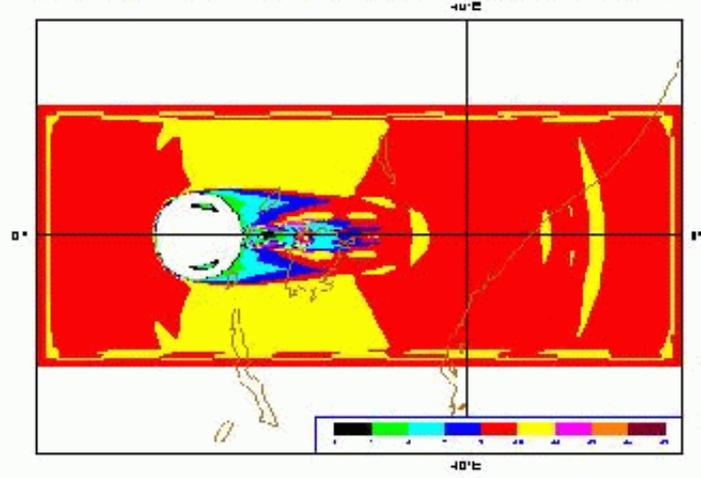
# 500M WITCH OF AGNESI



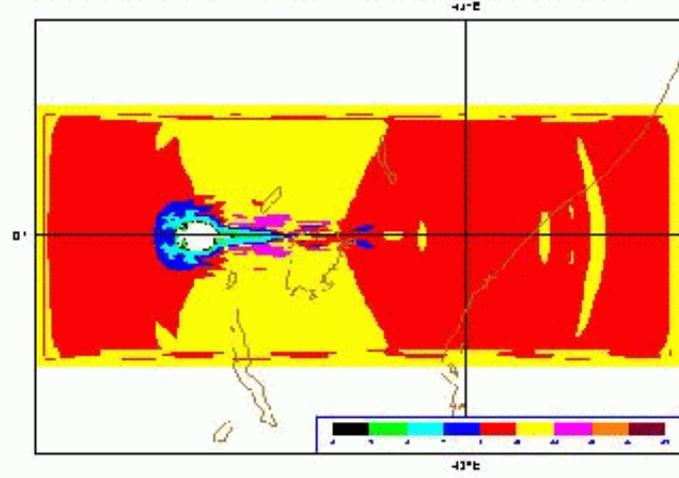
# 500M RECTANGULAR CUBE



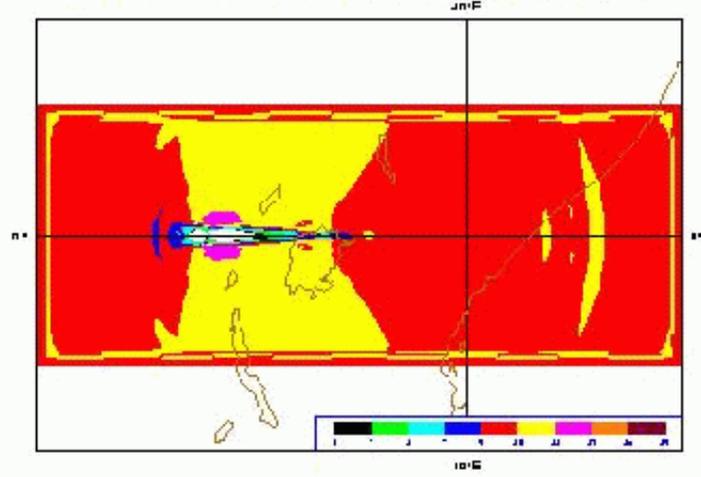
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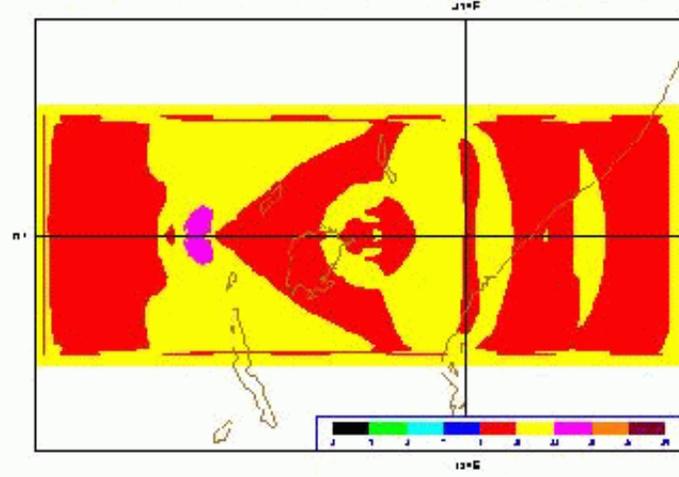
Monthly 1800-mbar-2000DUTCHORVAL - Period: 01-VI-Tuesday 17-06-2016-2000DUTCHORVAL Level: 2000DUTCHORVAL Unit: 1000DUTCHORVAL



Monthly 1800-mbar-2000DUTCHORVAL - Period: 02-VI-Wednesday 17-06-2016-2000DUTCHORVAL Level: 2000DUTCHORVAL Unit: 1000DUTCHORVAL



Monthly 1800-mbar-2000DUTCHORVAL - Period: 03-VI-Thursday 17-06-2016-2000DUTCHORVAL Level: 2000DUTCHORVAL Unit: 1000DUTCHORVAL



## Closing remarks

1. Couples grid-scale and sub-grid scales to the larger scales by allowing for sub-grid processes without directly modelling them.
2. An alternative treatment of the lower boundary by adding resistance to the flow.
3. Include low-level drag or blocking into the dynamics rather than the parametrizations OR parametrizations can be made 3 dimensional.
4. Handle complex geometries (walls, edges, buildings, trees, etc.) in environmental flows.
5. Easy to build terms into model (UM branch available) and can be used with terrain-following coordinates.

## References

- Smolarkiewicz et al (2007) J. Comp. Phys. “Building resolving LES and comparisons with wind tunnel experiments” - the building is the Pentagon!
- Smolarkiewicz and Winter (2010) J. Comp. Phys. “Pores resolving simulation of Darcy flows” - porous media



