

A semi-implicit non-hydrostatic covariant dynamical kernel using spectral representation in the horizontal and a height based vertical coordinate

Juan Simarro and Mariano Hortal  
AEMET Agencia Estatal de Meteorología, Spain

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# 3D model dynamical core

## Main characteristics

- Hybrid vertical coordinate based on height
- Finite differences in the vertical
- Covariant formulation
- Spectral discretization in the horizontal
- Semi-implicit time discretization
- Eulerian or semi-Lagrangian advection

# Euler equations for the dry air case

## Euler equations

$$\begin{aligned}\frac{d\mathbf{v}}{dt} + RT \nabla q + \nabla \phi &= \mathbf{F} \\ \frac{dr}{dt} + \frac{R}{C_v} (\nabla \cdot \mathbf{v}) &= \frac{Q}{C_v T} \\ \frac{dq}{dt} + \frac{C_p}{C_v} (\nabla \cdot \mathbf{v}) &= \frac{Q}{C_v T}\end{aligned}$$

- Prognostic variables are  $q = \ln p$ ,  $r = \ln T$  and  $\mathbf{v} = (u, v, w)$

$T$  is the temperature,  $p$  the pressure  $\mathbf{v}$  the velocity vector,  $R$  is the gas constant for dry air,  $C_p$  the specific heat capacity of dry air at constant pressure,  $C_v$  the specific heat capacity of dry air at constant volume,  $\mathbf{F}(t, \mathbf{x}, z)$  is the diabatic momentum forcing,  $Q(t, \mathbf{x}, z)$  the heat per unit mass and unit time added to the air,  $\phi(z) = gz$  the geopotential,  $\nabla \phi$  the gradient of geopotential,  $\nabla q$  the gradient of the logarithm of pressure and  $\nabla \cdot \mathbf{v}$  the divergence of the velocity

# Prognostic variables

## Why $q \equiv \ln p$ and $r \equiv \ln T$ ?

- Ideal state equation is linear in  $q$ ,  $r$  and  $\ln \rho$

$$q = r + \ln \rho + \ln R$$

- Prognostic equations for  $q$  and  $r$  are **linear** in prognostic variables in the adiabatic case and have the **same forcing** terms

$$\frac{dr}{dt} + \frac{R}{C_v} (\nabla \cdot \mathbf{v}) = \frac{Q}{C_v T}$$

$$\frac{dq}{dt} + \frac{C_p}{C_v} (\nabla \cdot \mathbf{v}) = \frac{Q}{C_v T}$$

- For a given **time and spatial discretization** of  $\dot{q}$ ,  $\dot{r}$  and  $\nabla \cdot \mathbf{v}$

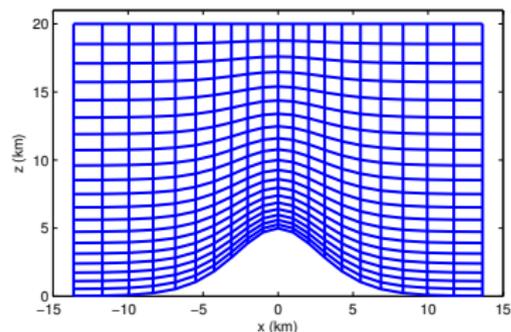
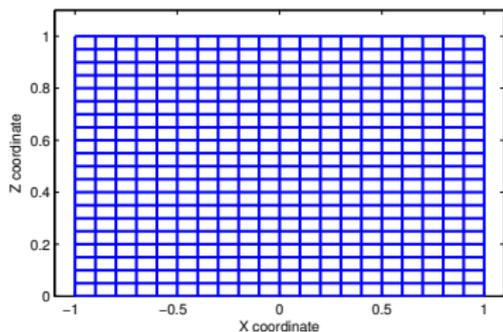
$$\frac{dq}{dt} - \frac{dr}{dt} = \frac{d}{dt}(q - r) \Rightarrow \frac{d \ln \rho}{dt} + \nabla \cdot \mathbf{v} = 0$$

# Model coordinates

- Cartesian  $(x, y, z)$  coordinates are transformed into model coordinates  $(X, Y, Z)$
- Vertical domain is  $Z \in [0, 1]$  and the horizontal domains are  $X \in [-1, 1]$  and  $Y \in [-1, 1]$ .
- The spatial domain in Cartesian coordinates is bounded by a rigid top at  $z = H_T$  and a rigid bottom at  $z = H_B(x)$

# Domains and grids of physical and model spaces

## Representation of the grid



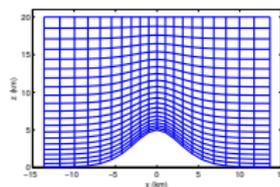
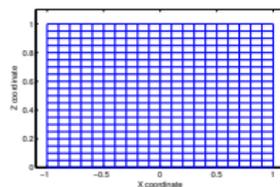
# Covariance

- The grid in the model coordinates is regular and it is not in Cartesian coordinates
- The relationship between both coordinates is **analytical and constant in time**
- The model is **covariant** in the sense that all the objects are expressed in model coordinates
- The **contravariant velocity** is chosen as prognostic variable instead covariant velocity because boundary conditions are simply  $W(X, Y, 0, t) = 0$  and  $W(X, Y, 1, t) = 0$
- Following differential geometry the covariant **metric tensor** in the new coordinates is all what is needed to express differential operators as divergence, gradient and curl

# Metric tensor

- The **metric tensor**  $G$  in the model coordinates is obtained with the help of the **Jacobian** of the coordinate transformation and the metric tensor in Cartesian coordinates which is the identity

$$G = J^T J$$



# Differential operators

- Differential operators are calculated from the metric tensor and its inverse ( $G_{ij}$ , and  $G^{ij}$ ) and the Christoffel symbols  $\Gamma_{jk}^i$

$$\Gamma_{jk}^i = \frac{1}{2} G^{im} \left( \frac{G_{mj}}{\partial X^k} + \frac{G_{mk}}{\partial X^j} - \frac{G_{jk}}{\partial X^m} \right)$$

- Divergence

$$\nabla \cdot \mathbf{v} = \frac{1}{|\det G|^{\frac{1}{2}}} \frac{\partial}{\partial X^j} \left( |\det G|^{\frac{1}{2}} U^j \right)$$

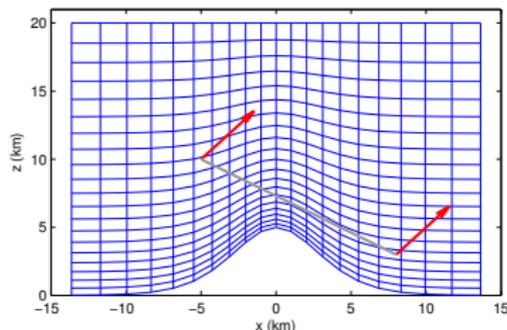
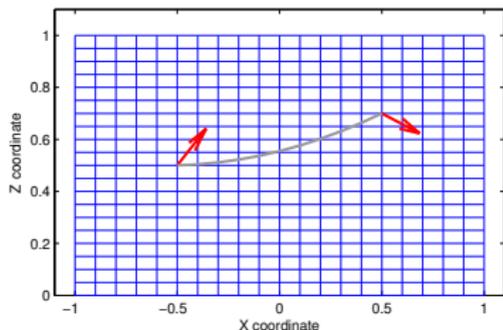
- Gradient

$$(\nabla f)^i = G^{ij} \frac{\partial f}{\partial X^j}$$

- Covariant derivative

$$(\nabla_{\mathbf{u}} \mathbf{v})^i = U^j \frac{\partial V^i}{\partial X^j} + \Gamma_{jk}^i U^j V^k$$

# Geodesic, parallel transport



- For the semi-lagrangian advection **parallel transport** is used for calculating the difference between contravariant vectors at the departure and arrival points
- The trajectory is calculated using a **geodesic** curve corresponding to the covariant metric tensor
- In this way the semi-lagrangian scheme has a **full covariant formulation**, in particular the physical velocity components are not used

# Vertical discretization

- A 2D VFE version has been coded (paper accepted for publishing at QJRMS, Simarro and Hortal)
- Here a 3D vertical finite differences (VFD) version is presented
- The prognostic variables are all in full levels except the contravariant vertical velocity which is in half levels plus two boundary levels where it is zero
- All the vertical discretization is second order, including those levels near the boundaries

# Vertical operators

Basically 4 operators are defined

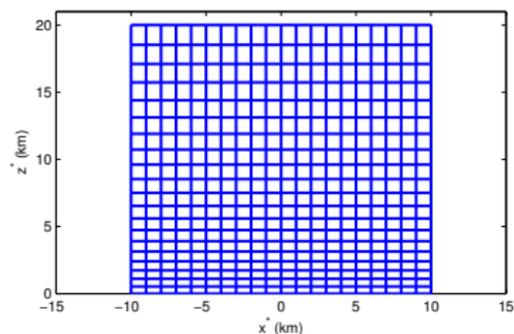
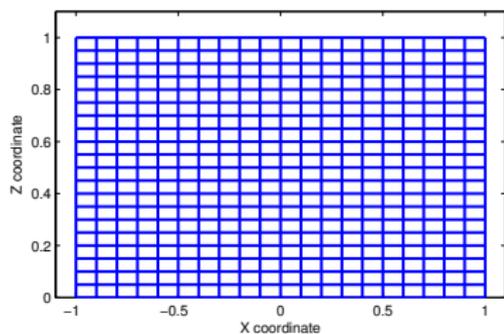
- $\mathbf{D}_Z$  finds the vertical derivative in full levels and the result is placed in half levels
- $\hat{\mathbf{D}}_Z$  finds the vertical derivative in half levels considering that the variable is zero at the boundaries and the result is placed in full levels
- $\mathbf{I}_Z$  finds the vertical linear interpolation from full levels to half levels
- $\hat{\mathbf{I}}_Z$  finds the vertical linear interpolation from half levels to full levels considering that the variable is zero at the boundaries

# Semi-implicit time discretization

- The semi-implicit formulation follows closely the formulation used in ALADIN with the **mass-based vertical coordinate**
- The linear model is around an isothermal hydrostatic balanced atmosphere at rest
- A **flat orography** is used in the reference state **instead of a constant hydrostatic pressure**

# Linear coordinates

- For the linear system another coordinate transformation is needed which is horizontally uniform
- From this transformation a **linear metric tensor**  $G^{Y*}$  is obtained. Consequently the differential operators of the linear model also change.



## 3TL semi-implicit scheme

- A 3TL level scheme is represented by the following equation

$$\frac{\mathbf{X}^{n+1} - \mathbf{X}^{n-1}}{2\Delta t} = \mathbf{M}(\mathbf{X}^n) - \mathbf{L}(\mathbf{X}^n) + \frac{1-\epsilon}{2}\mathbf{L}(\mathbf{X}^{n-1}) + \frac{1+\epsilon}{2}\mathbf{L}(\mathbf{X}^{n+1})$$

- $\mathbf{M}$  is the non linear model and  $\mathbf{L}$  the linear model
- $\epsilon$  is a decentering factor which increases stability
- $\mathbf{X} = (\mathbf{U}, \mathbf{V}, \mathbf{W}, \mathbf{r}, \mathbf{q})$  is the state vector
- The linear system is solved for  $\mathbf{X}^{n+1}$  in the spectral space

# Linear model

$$\frac{\partial \mathbf{U}}{\partial t} + \frac{RT^*}{m_X^2} \mathbf{D}_X \mathbf{q} = 0$$

$$\frac{\partial \mathbf{V}}{\partial t} + \frac{RT^*}{m_Y^2} \mathbf{D}_Y \mathbf{q} = 0$$

$$\frac{\partial \mathbf{W}}{\partial t} + \frac{RT^*}{m_Z^2} \mathbf{D}_Z \mathbf{q} - \frac{g}{m_Z} \mathbf{I}_Z \mathbf{r} = 0$$

$$\frac{\partial \mathbf{r}}{\partial t} + \frac{R}{C_v} \left( \mathbf{D}_X \mathbf{U} + \mathbf{D}_Y \mathbf{V} + \hat{\mathbf{D}}_Z \mathbf{W} \right) = 0$$

$$\frac{\partial \mathbf{q}}{\partial t} + \frac{C_p}{C_v} \left( \mathbf{D}_X \mathbf{U} + \mathbf{D}_Y \mathbf{V} + \hat{\mathbf{D}}_Z \mathbf{W} \right) - \frac{m_Z g}{RT^*} \hat{\mathbf{I}}_Z \mathbf{W} = 0$$

- $m_X^2$ ,  $m_Y^2$  and  $m_Z^2$  are the diagonal elements of the linear metric tensor

# Structure equation

- The following structure equation is obtained, which is similar to the structure equation of the ALADIN model

$$(\mathbf{I} - \beta^2 c_*^2 (\mathbf{D}_X^2 + \mathbf{D}_Y^2 + \mathbf{L}_Z) - \beta^4 c_*^2 N_*^2 (\mathbf{D}_X^2 + \mathbf{D}_Y^2) \mathbf{T}_Z) \mathbf{W}^{n+1} = \mathbf{R}_C$$

- where  $\mathbf{L}_Z$  and  $\mathbf{T}_Z$  are vertical operators which contains vertical derivatives and linear interpolations operators and the constants are

$$c_*^2 = \frac{C_p}{C_v} RT^*$$

$$N_*^2 = \frac{g^2}{C_p T^*}$$

$$H_* = \frac{RT^*}{g}$$

$$\beta = (1 + \epsilon) \Delta t$$

## Differences with the mass based vertical coordinate

- Contrary to the case of the mass-based vertical coordinate **no constraints have to be fulfilled by the vertical operators** when deriving the structure equation
- **There is not a  $X$  term** in the divergence due to the use of the contravariant vertical velocity
- The **boundary conditions for the contravariant vertical velocity are included in the vertical operators and are automatically fulfilled**
- A disadvantage is that the **decentering factor must be greater than zero for achieving a similar range of stability (according to the SBH method) than the one obtained with the mass-based coordinate**

# Test

## Following test have been done among others

- Atmosphere at rest with inversion layer (Klemp, 2011)
- Inertia-gravity wave test (Klemp and Skamarock, 1994)
- 3D flow over a hill (Smith, 1980)
- Conservation of potential vorticity

## Configuration

- Decentering factor is  $\epsilon = 0$
- Reference temperature is  $T^* = 350 K$
- In some test there is an absorber layer in the upper part of the domain to avoid the reflection of gravity waves

# Rest atmosphere test

## Atmosphere at rest test from Klemp (2011)

- Consist of an atmosphere at rest with a horizontally homogeneous thermodynamic sounding and an orography described in Schär (2002)
- Although the atmosphere is initially in equilibrium at rest an **artificial circulation appears** during the integration due to numerical **pressure gradient errors**
- In Klemp (2011) it is used the model described in Klemp et al (2007) with a conservative time-explicit method
- The **Gal-Chen** (1975) vertical coordinate produced artificial circulations with maximum vertical velocities of  $7 \text{ m s}^{-1}$
- More sophisticated vertical coordinates results in smaller spurious circulations

# Rest atmosphere test: configuration

## Configuration

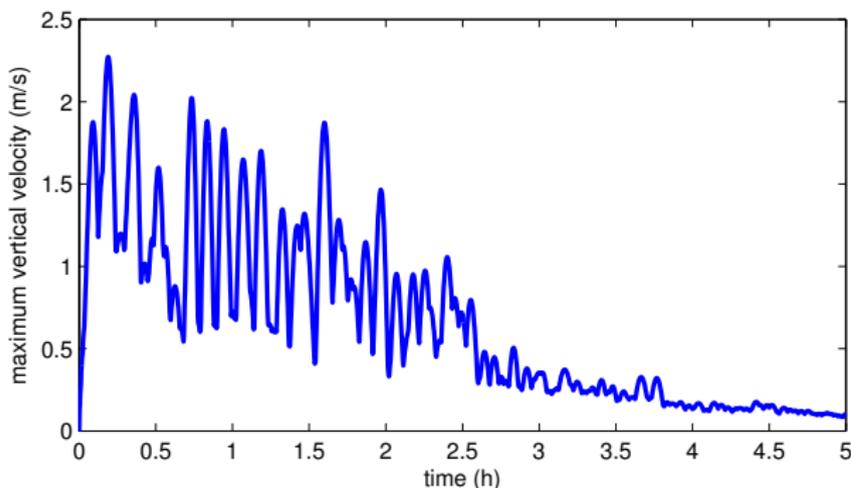
- Constant stability with an inversion layer:  $N = 0.01 \text{ s}^{-1}$  except  $N = 0.02 \text{ s}^{-1}$  from  $2 \text{ km}$  to  $3 \text{ km}$  height
- Schärer mountain:  $H_0 = 1 \text{ km}$ ,  $a = 5 \text{ km}$  and  $b = 4 \text{ km}$

$$H_B(x) = H_0 \exp\left(-\frac{x^2}{a^2}\right) \cos^2\left(\frac{\pi x}{b}\right)$$

- Coarse resolution:  $\Delta x = \Delta z = 500 \text{ m}$
- Gal-Chen vertical coordinate and top placed at  $20 \text{ km}$
- Diffusion coefficient:  $15 \text{ m}^2 \text{ s}^{-1}$
- No vertical sponge zone and cyclic conditions in the horizontal
- Time step  $\Delta t = 10 \text{ s}$

## Rest atmosphere test: maximum vertical velocities

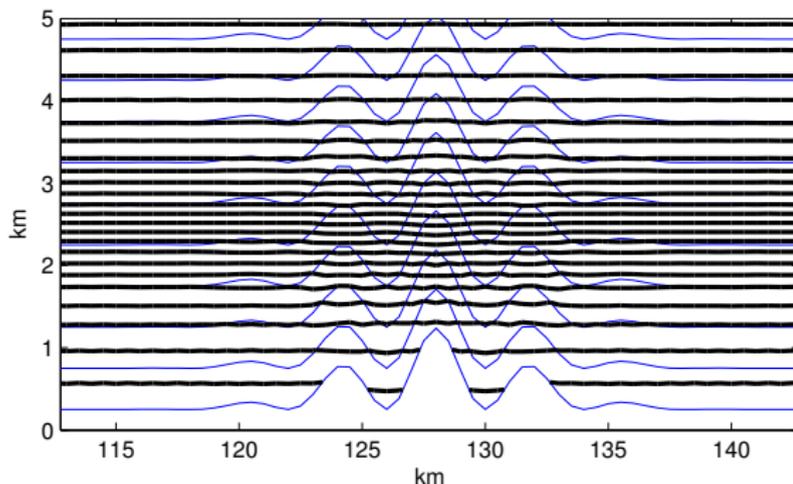
- Atmosphere is initially in equilibrium at rest but artificial circulation appears during the integration due to numerical pressure gradient errors



Maximum vertical velocity during the first 5 hours

# Rest atmosphere test: potential temperature distortion

- $\theta$  isolines are initially horizontal and they are slightly distorted by the spurious circulations



$\theta$  after 5 hours of integration and full model levels in blue

# Inertia-gravity waves test

## Test case found in Skamarock and Klemp (1994)

- There the efficiency and accuracy of the Klemp-Wilhelmson time splitting technique is explored and a propagating inertia-gravity wave is simulated in a Boussinesq atmosphere with constant stability parameter in a periodic channel with solid, free-slip upper and lower boundaries
- The waves are produced by an initial potential temperature perturbation where a small amplitude  $\Delta\theta_0 = 0.01 K$  is chosen for quantitative comparisons with the analytic solutions of the linearized equations

$$\theta(x, z, 0) = \Delta\theta_0 \frac{\sin(\pi z)}{1 + \left(\frac{x-x_0}{a}\right)^2}$$

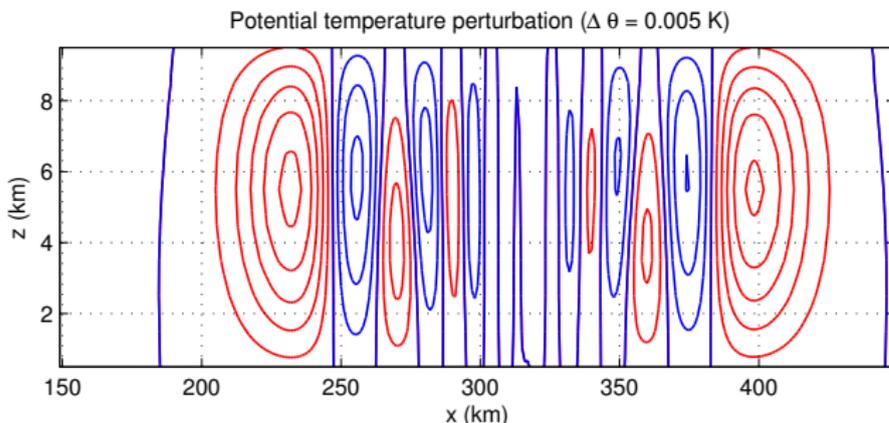
# Inertia-gravity waves test: configuration

## Configuration

- Constant stability parameter  $N = 0.01 \text{ s}^{-1}$
- Upper boundary at  $H_T = 10 \text{ km}$
- Perturbation half width is  $a = 5 \text{ km}$
- Initial horizontal velocity is  $U = 20 \text{ ms}^{-1}$
- Horizontal and vertical resolutions are  $1000 \text{ m}$
- Time step is  $\Delta t = 6 \text{ s}$ .

# Inertia-gravity waves test: results

- The numerical solution for  $\theta$  at 3000 s are similar to the analytical solution, although there is a vertical movement which is not present in the linear Boussinesq solution



## Linear 3D wave test

- Smith (1980) found linear solutions of steady flows which are used here to compare with the nonlinear model solutions

### Consider

- steady-state small-amplitude stratified Boussinesq flow
- adiabatic, inviscid and nonrotating
- uniform basic velocity  $U$  and Brunt-Vaisala frequency  $N$
- three dimensional topography  $H_B(x, y)$

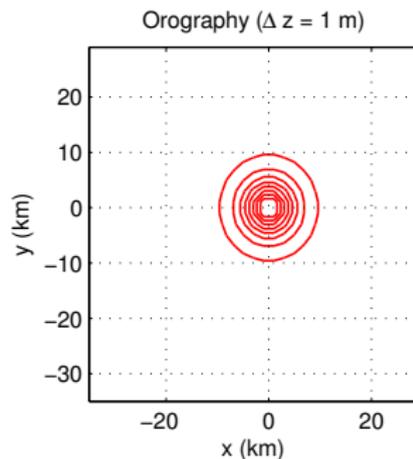
Then the vertical displacement  $\eta(x, y, z)$  is given by

$$\left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) \frac{\partial^2}{\partial x^2} \eta + \frac{N^2}{U^2} \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \eta = 0$$

# Linear 3D wave test: configuration

Orography:  $H_0 = 10 \text{ m}$  and  $a = 5 \text{ km}$

$$H_B(x, y) = \frac{H_0}{\left(1 + \frac{x^2 + y^2}{a^2}\right)^{2/3}}$$



# Linear 3D wave test: configuration

## Basic state

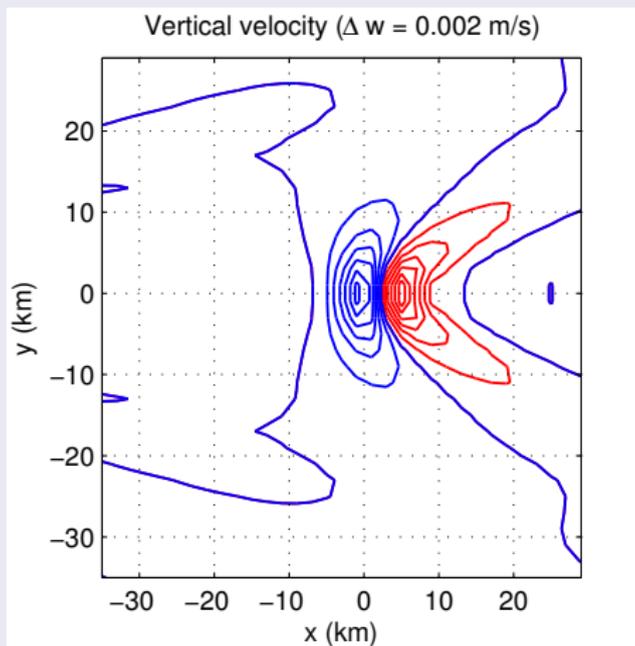
- $u = 10 \text{ m s}^{-1}$  and  $N = 0.01 \text{ s}^{-1}$

## Grid and resolution

- Domain:  $64 \times 64$  grid points in the horizontal and 40 levels
- Resolution:  $\Delta x = \Delta y = 2 \text{ km}$  and  $\Delta z = 500 \text{ m}$

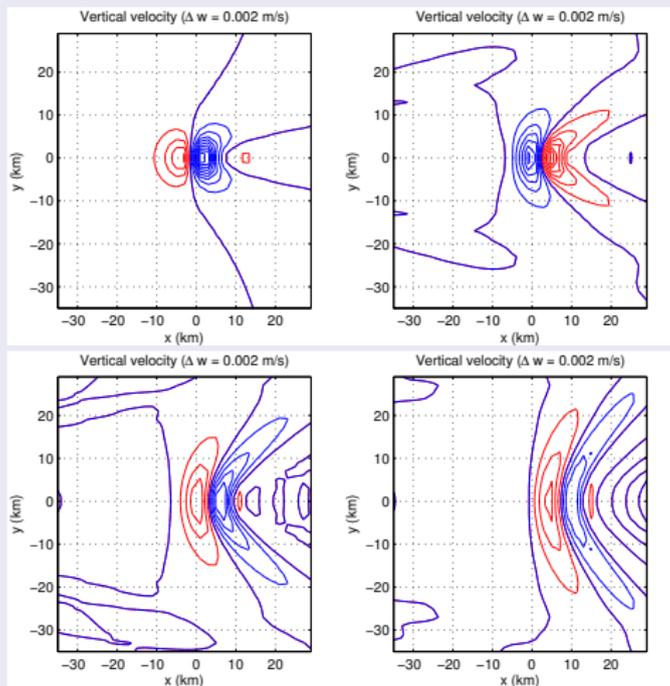
# Linear 3D wave test: linear solution

## Linear vertical velocity at level 4 following Smith (1980)



# Linear 3D wave test: linear solution

## Linear vertical velocity at levels 1, 4, 10 and 20



# Linear 3D wave test: non linear solution

## Configuration

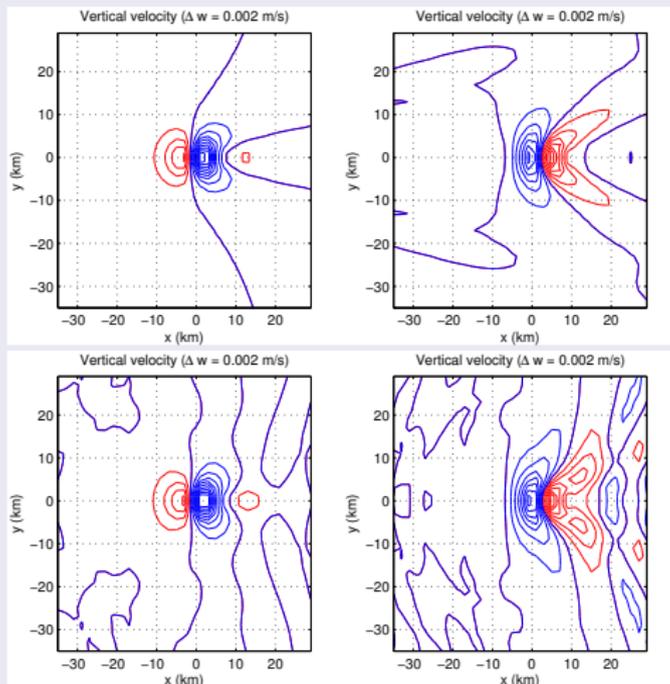
- Same grid used for the linear solution
- Top at  $20 \text{ km}$
- Time step:  $\Delta t = 20 \text{ s}$ ,  $\epsilon = 0$
- Reference temperature:  $350 \text{ K}$
- Cyclic conditions in the horizontal dimensions
- Sponge layer at the highest  $4 \text{ km}$  of the domain
- Results presented at  $T = 30000 \text{ s}$

## Attention!

- Linear and non linear solutions must be not equal as they obey different equations

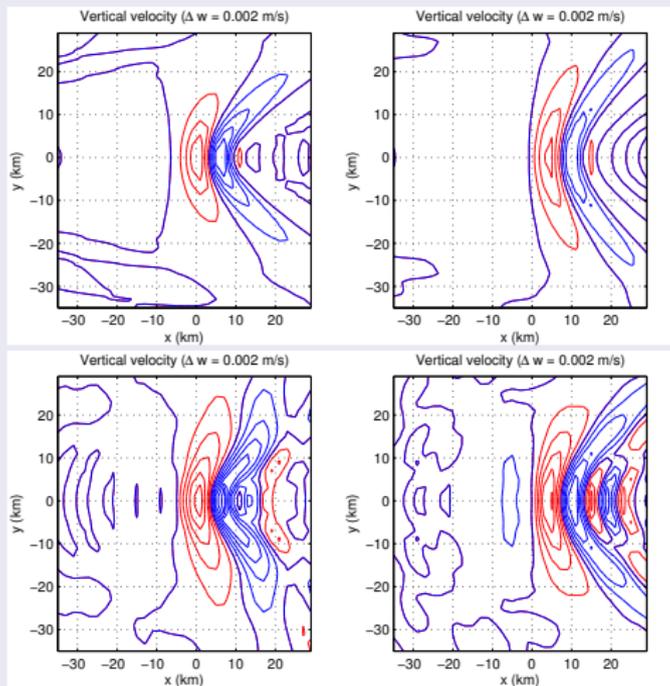
# Linear 3D wave test: non linear solution

## Linear and non linear vertical velocities at levels 1 and 4



# Linear 3D wave test: non linear solution

## Linear and non linear vertical velocities at levels 10 and 20



# Potential vorticity conservation

## Preliminary test to evaluate potential vorticity conservation

- A flow with constant  $U = 10 \text{ m s}^{-1}$  and  $N = 0.01 \text{ s}^{-1}$  passes around an 3D Agnesi hill  $a = 5 \text{ km}$  and  $H_0 = 500 \text{ m}$ .
- The flow has **zero potential vorticity upstream the hill** and should conserve this value in an adiabatic flow
- The potential vorticity is calculated at  $T = 3200 \text{ s}$
- Two cases: **adiabatic** case and **non adiabatic** with heat source. The heat source is proportional to the orography and constant with height, therefore the hill acts like a chimney

# Potential vorticity conservation

## How to find potential vorticity

- The covariant expression for the potential vorticity is

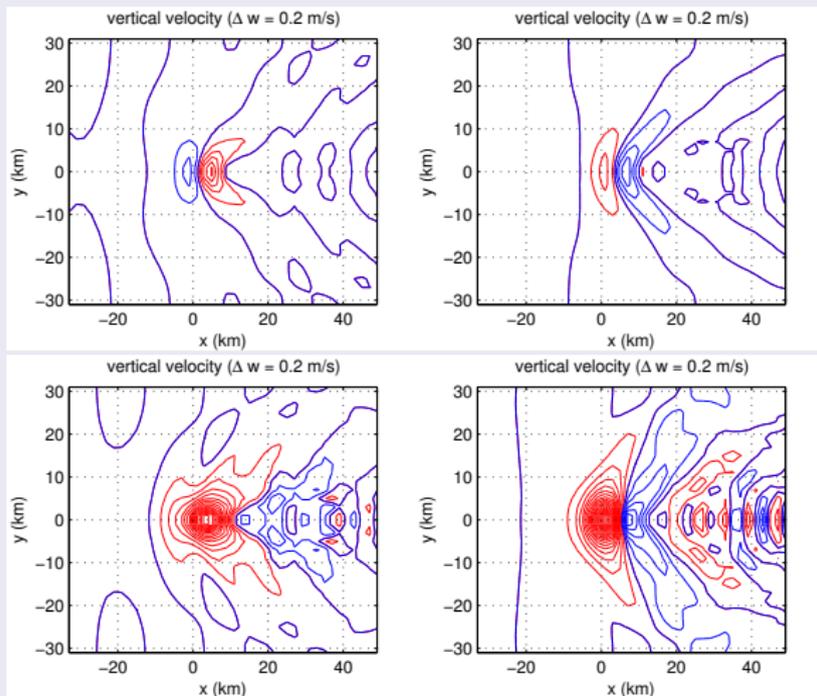
$$PV = \frac{1}{\rho|G|^{\frac{1}{2}}} \left( \theta_X \left( \hat{V}_Z - \hat{W}_Y \right) + \theta_Y \left( \hat{W}_X - \hat{U}_Z \right) + \theta_Z \left( \hat{U}_Y - \hat{V}_X \right) \right)$$

where  $\hat{U}$ ,  $\hat{V}$  and  $\hat{W}$  are the covariant components of the velocity

- Vertical and horizontal derivatives are calculated with respect model coordinates

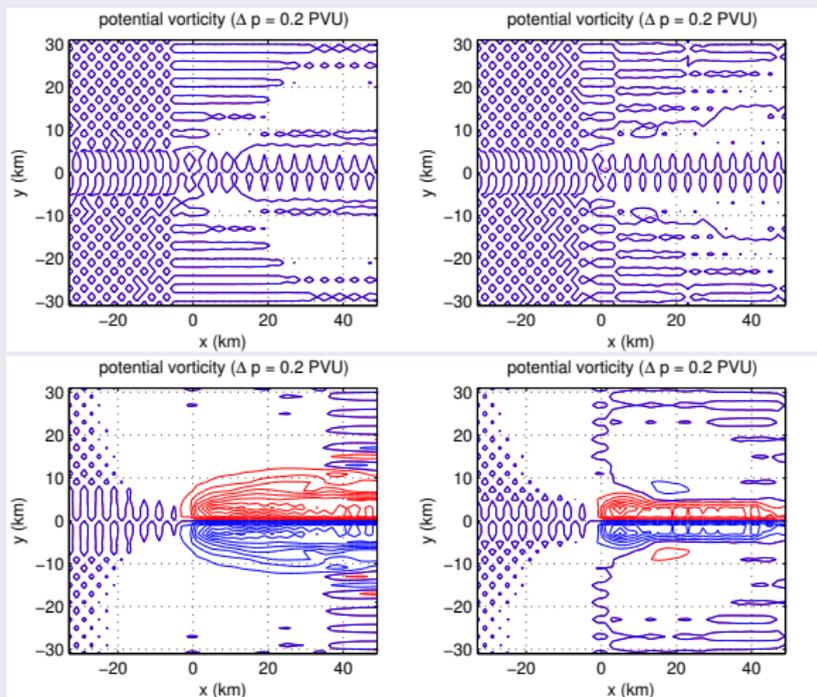
# Potential vorticity conservation

Vertical velocity at 2.5 and 5.0 *km* height (adiabatic flow up)



# Potential vorticity conservation

Potential vorticity at 2.5 and 5.0 km height (adiabatic flow up)



# Conclusions

- A 3D VFD model has been coded and tested
- The scheme is robust
- This formulation has some advantages in front of the mass based vertical coordinate
- A preliminary potential vorticity test has been done

# Questions (?) and answers (!)

- Work already done in the IFS/HARMONIE code?
  - Preparing initial data in  $Z$  coordinate
  - Vertical operators
  - Part of the modifications in the semi-implicit solver
- VFE or VFD?
  - robustness(VFD) > robustness(VFE)
  - VFD to be implemented first
- LAM/Global?
  - First implemented in Global to avoid lateral boundaries

Thank you for your attention!